



# **Hard Chrome Alternatives Team - Tri-Service Validation of HVOF Thermal Spray as a Chrome Replacement for Aircraft**

**Bruce Sartwell**

**Naval Research Lab**

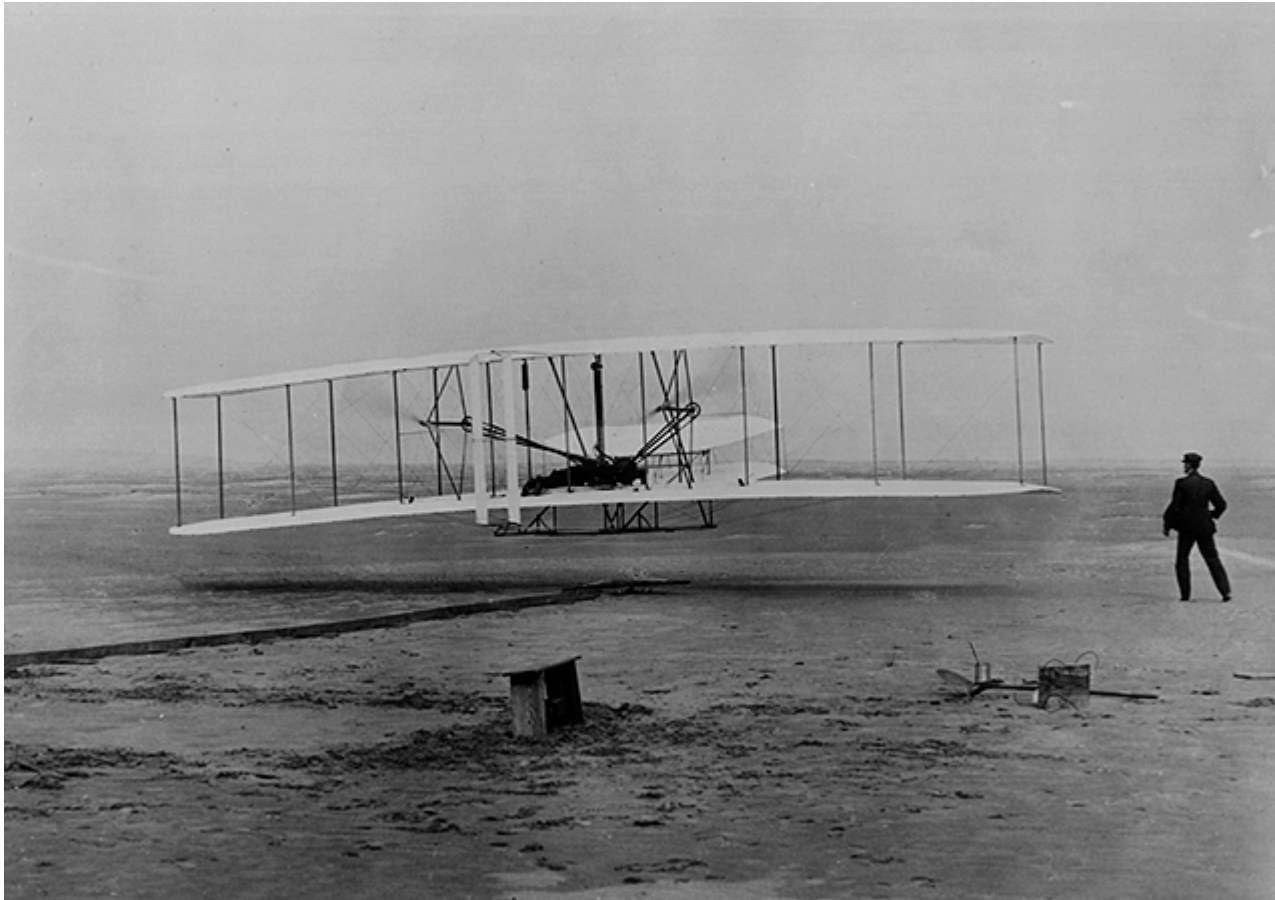
**Keith Legg**

**Rowan Technology Group**

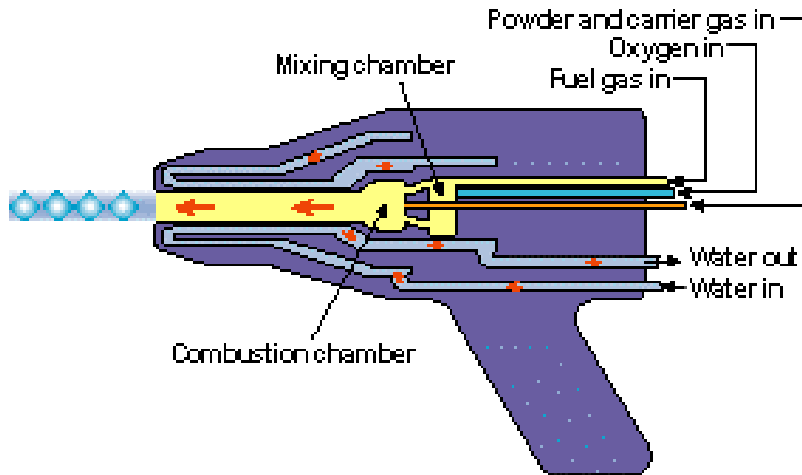
**RUST 2001**

# The last aircraft made without Cad and hard Cr

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# HVOF process



- **Supersonic fuel-oxygen flame (H<sub>2</sub>, kerosene, ethylene, acetylene)**
- **WC-Co or alloy powder**

# Successful replacements - specs and qualified components

## ■ Specifications

- BAC 5851 - new version
- HS 4412
- AMS 2447
- New AMS specs for powders, coating, finishing expected 2000 - 2001

## ■ Qualifications - new items

- Boeing > 100 airframe components spec'd for thermal spray
- Boeing 767-400 has landing gear spec'd for HVOF WC-CoCr
- **Bombardier Q400, Global Express flap tracks HVOF, replacing electroless Ni**
- **Hamilton Sundstrand - F-22 thrust vectoring actuator**
- **Parker - no Cr on new hydraulic actuator**



# Qualifications - repair

- **Boeing - HVOF approved for LG repair up to 0.010"**
  - Boeing evaluating thick build-up methods
- **Delta - approved HVOF for landing gear repair**
  - inner cylinders and axles
- **United - moving toward in-house HVOF for LG**
- **F-18 polygon repair**
- **TWI (UK) L-1011 Ti flap track repair (weld + HVOF WC-Co)**



# Purpose of the HCAT program

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- **Demonstrate and validate HVOF coatings for replacement of hard chrome on aircraft systems**
- **Incorporate all the major stakeholders to ensure that the data will lead to approval**
  - **Get all the relevant technical data**
  - **Address all major producibility issues - grinding, finishing, stripping, O&R compatibility**



Environmental Security  
Technology Certification  
Program

# Approach

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## ■ Stakeholders

- **Agreement to Joint Test Protocol by all major stakeholders**
  - ❑ **Approval authorities (NAVAIR, ATCOM, etc.)**
  - ❑ **OEMs (Boeing, Lockheed, Goodrich, etc.)**
  - ❑ **Depots (ALCs, NADEPs, Army depots)**
    - **include technical, management**

■ **Across-the-board change will not be accepted, item-by-item too slow and expensive**

## ■ Attack by sub-system

- **common stakeholders**
- **common technical issues**
- **limited number of bases, suppliers**

## ■ Implementation

- **Single process initiative**

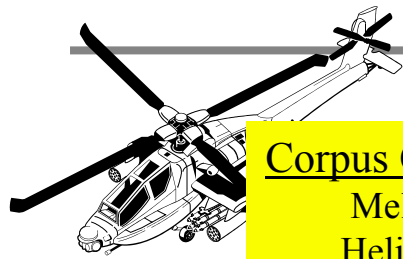
# HCAT - aircraft systems being validated

- **Landing gear**
  - **Close to completion**
- **Propeller hubs**
  - **Close to completion**
- **Hydraulic actuators**
  - **Just starting - JTP being developed**
- **Gas turbine engines**
  - **JTP almost complete**
- **Helicopter head components**
  - **Planned**



# HCAT - US Team

**Note: All depots have HVOF  
 Depot training by GEAE**



Corpus Christi AD  
 Mel Avila  
 Helicopters

NADEP Jax  
 Jon Deveraux  
 Navy aircraft

GE Aircraft Engines  
 Jerry Schell  
 OEM - Engines  
 Process development

NRL -Prog. Manager  
 Bruce Sartwell  
 Financial  
 Materials analysis



Southwest AeroService  
 Jim Nuse  
 HVOF and chrome

Metcut  
 John Sauer  
 Mech. tests

NADEP Cherry Point  
 Robert Kestler  
 Navy aircraft

JG-PP  
 Warren Assink  
 Single Process  
 Initiative

PEWG  
 Chuck Alford  
 Engines

Rowan -Tech. Lead  
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 Doug Wiser  
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 Landing gear

Hamilton Sundstrand  
 Aaron Nardi  
 Propeller hubs

NDCEE  
 Eric Brooman  
 Stripping

Praxair  
 John Quets

Engelhard  
 Peter Ruggiero

Hitemco  
 Ed Garofolo  
 HVOF

OC-ALC  
 Mike O'Donnell  
 Engines

Boeing  
 Dennis Dull  
 John Falkowski  
 Embrittlement, impact

Sulzer Metco  
 Bruce Bodger

# C-HCAT - Canadian Team



BF Goodrich  
 Roque Panza-Giosa  
 Dash 8  
 Hydraulic rig tests



Industry Canada  
TPC  
 Lawrence Otupiri  
 Funding

DND  
 Mike Janowicz  
 Testing support

Orenda  
 Jason Dyer  
 Coupon testing

Messier-Dowty  
 Roger Eybel  
 F-18 rig tests

Rowan  
 Keith Legg  
 Coordination  
 Data integration

Heroux  
 Nihad Ben-Salah  
 C-130  
 Producibility

Vac-Aero  
 Jeff Pritchard  
 HVOF

NRC  
 Jean-Gabriel Legoux  
 Process development

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**Data being generated**

**Mostly landing gear**

# Materials

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## ■ Substrates

- 4340
- 300M
- Aermet 100
- Early evaluations included
  - ❑ 7075-T6 Aluminum
  - ❑ PH 13-8Mo
  - ❑ IN 718
- **GTE evaluations will include IN 718, IN 901, AMS355, A286, 17-4PH, 4340, 9310**

## ■ Coatings

- WC-17Co
  - WC-10Co4Cr
  - Tribaloy 400, 800
- ## ■ GTE evaluations will include $\text{Cr}_3\text{C}_2$ -(Ni, Cr)
- Note: these are based on experience and are not the only options**

# How good is Cr anyway?

- **Aircraft industry has long experience but very little hard data**
  - good adhesion, wear, lubricity
  - very variable quality
  - significant fatigue debit
  - not useful for corrosion protection (microcracks)
  - hydrogen embrittlement and rapid environmental embrittlement

- **Hard chrome has been in production since 1928**
- **But Cr is not the cat's pajama**



## Results

**Optimization** - common guns, fuels  
**Properties** - structure, hardness, adhesion  
**Performance:**

**Fatigue**

**Corrosion**

**Wear**

**Impact**

**Embrittlement**

**Rig tests**

**landing gear fatigue, endurance**

**hydraulic cylinder**

**turbine engine**

**propeller hub**

**Flight tests (commercial, DoD)**

# User requirements - landing gear

## ■ Commercial

- Typically 100 ksi, R=0.1, thousands of cycles
- Maximum 170 ksi, R=0.1

## ■ Land-based military

- 190 ksi, R=-0.33, 1,000cycles (Air Force)

## ■ Carrier-based military

- NLG Pins 235 ksi launch loads, R=-0.5, 2,250 cycles, (OEMs)

## ■ OEMs

- 0.003"

## ■ Airlines

- 0.010" or thicker for MRO

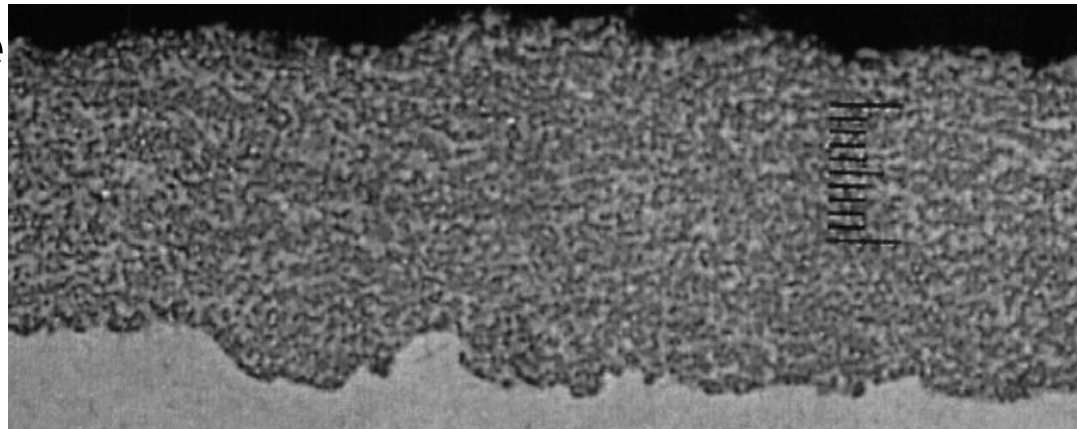
## ■ Repair Depots

**Yield stresses:**  
**4340M = 220 ksi**  
**300M = 230 ksi**  
**A100 = 235 ksi**



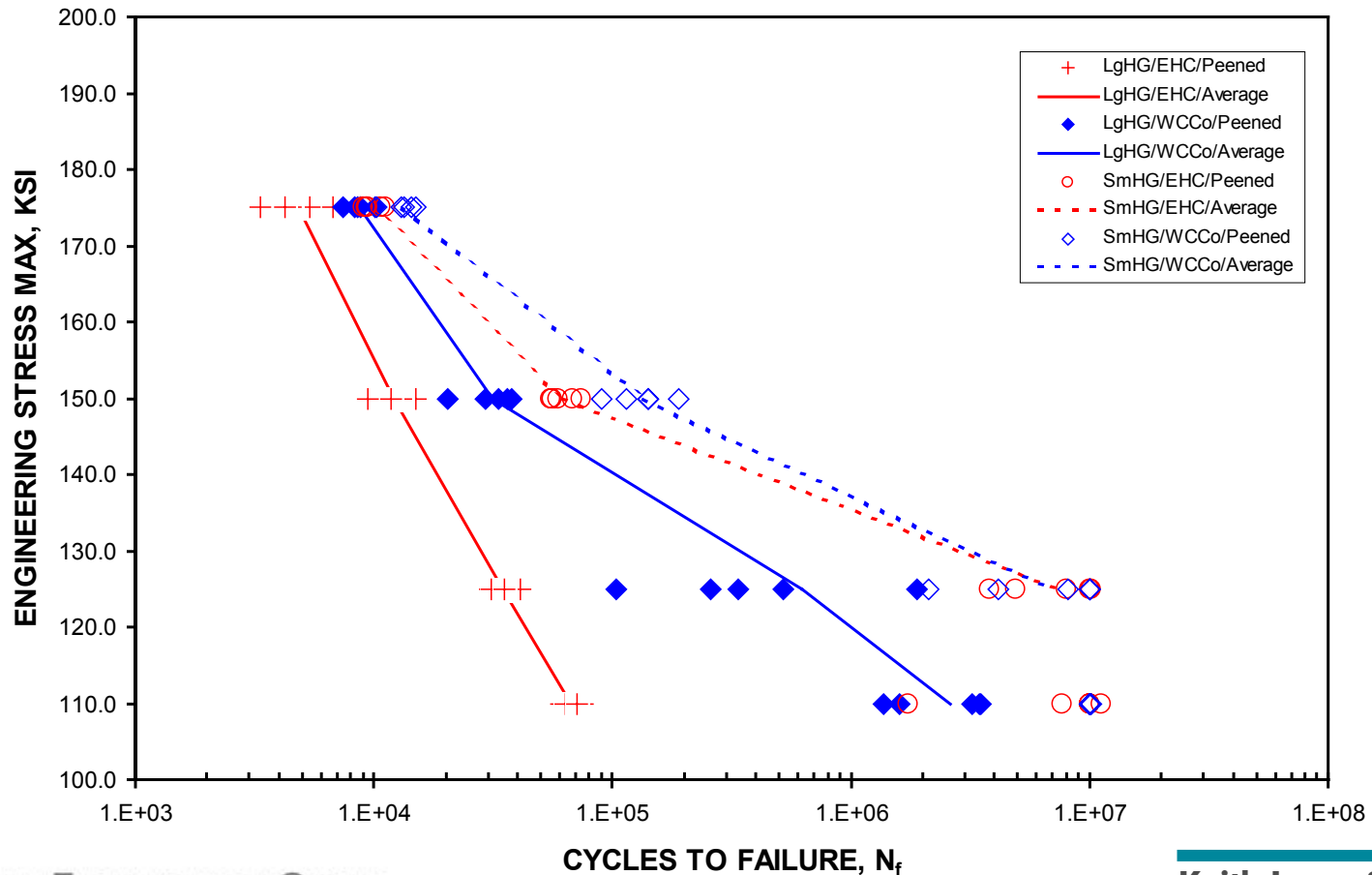
# Process development

- **WC-Co, WC-CoCr, T400 processes developed by Design of Experiment**
  - **Porosity - <1% to minimize corrosion and hydraulic leakage**
  - **Stress - compressive to minimize fatigue debit**
  - **Substrate softening**



# HCAT Landing gear fatigue - 4340

4340, R = -1, AIR  
 LARGE (0.010"CTNG) VS. SMALL (0.003"CTNG) HOURGLASS



# Fatigue summary

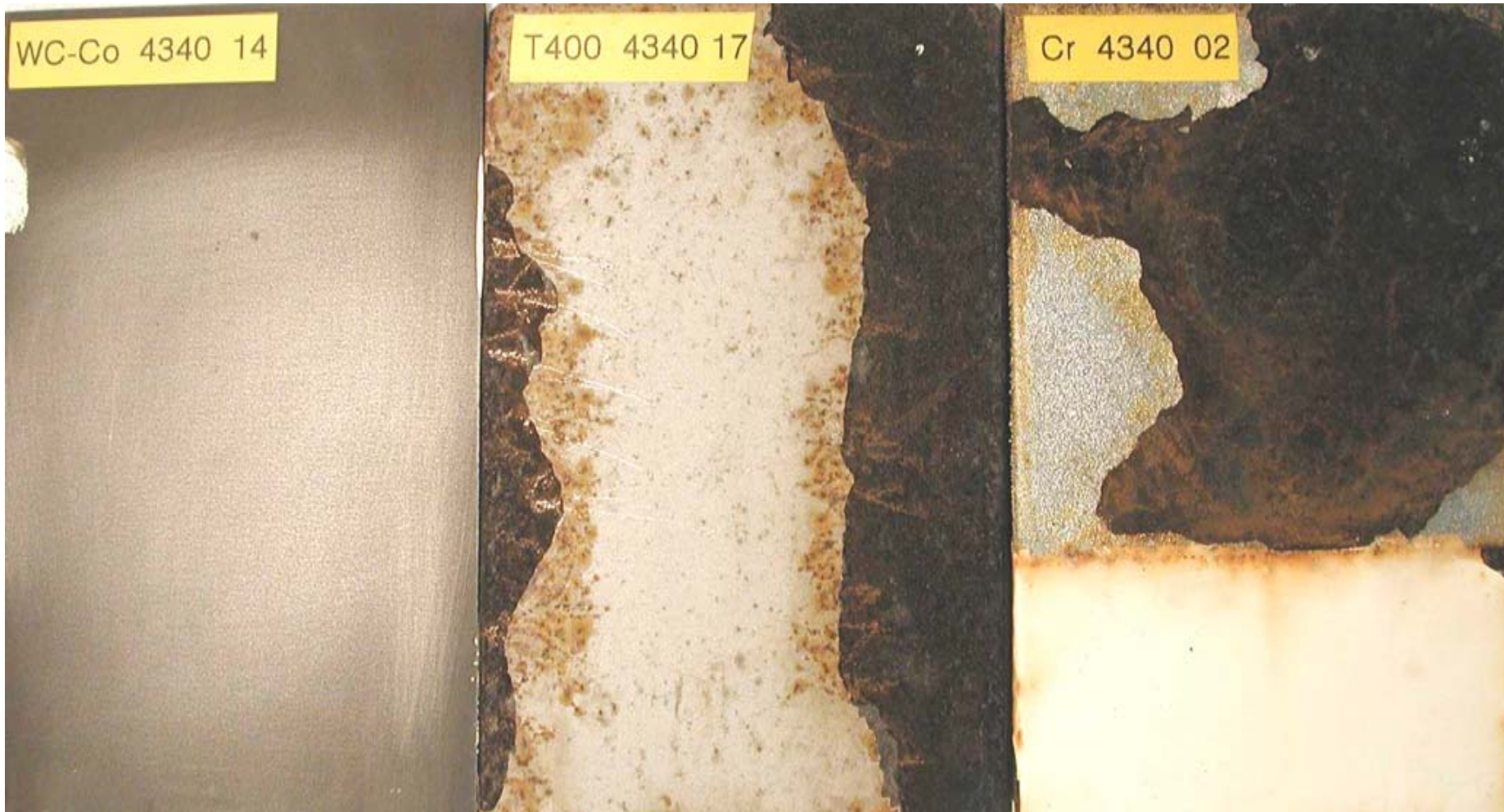
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- **HVOF can greatly reduce, or even eliminate, fatigue debit**
  - **Process definition and control are very important**
    - ❑ **Must ensure compressive residual stress in coating and avoid overheating**
  - **Coatings crack at high stress, but fatigue and corrosion fatigue remain excellent**
    - ❑ **Chrome is already cracked, of course**
  - **WC-Co and WC-CoCr coatings are brittle, and can spall if used under high stress**
    - ❑ **Appears significant only for carrier aircraft landing**

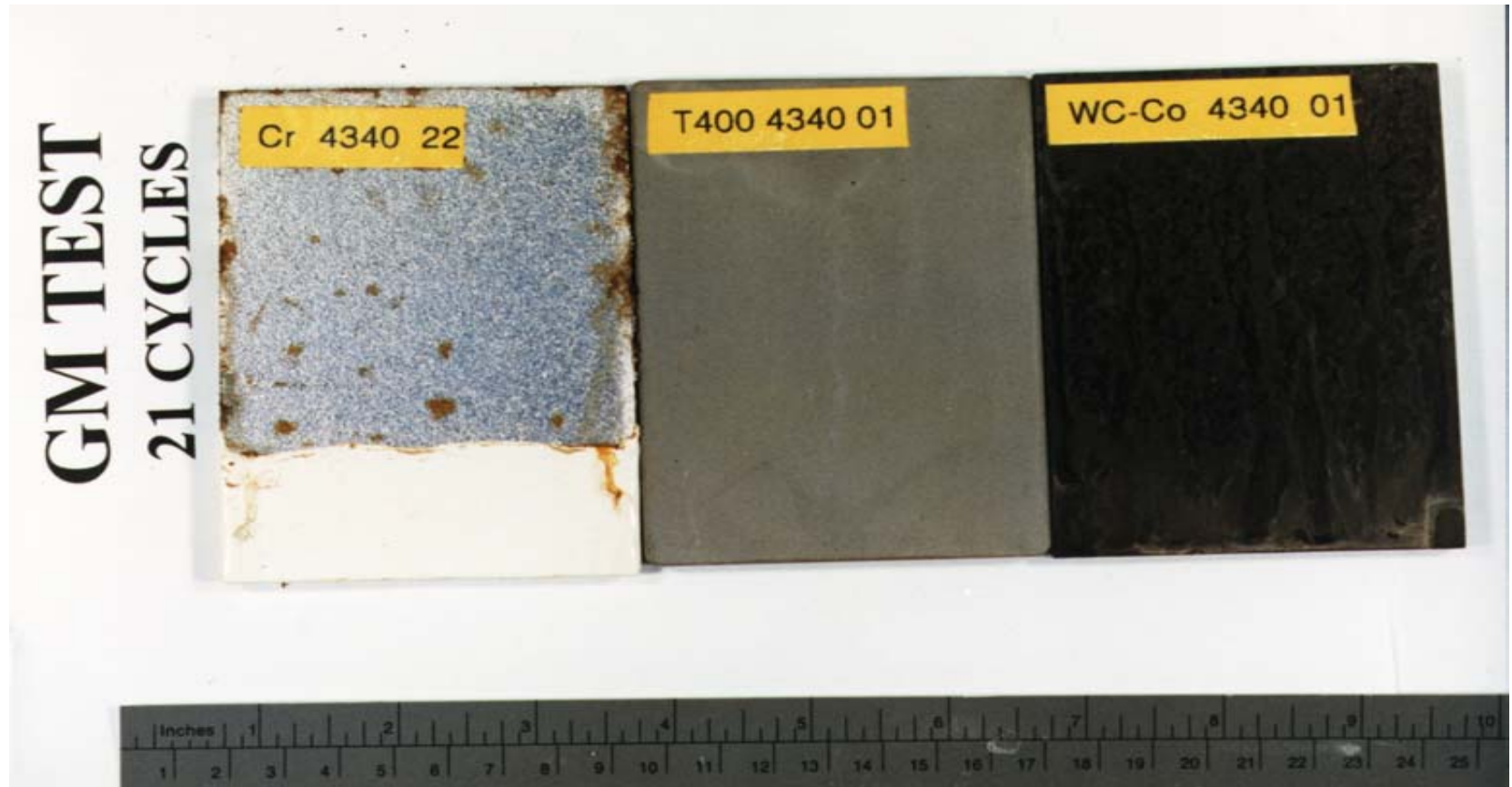
# Corrosion - early B117 data



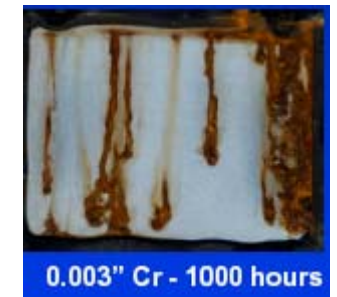
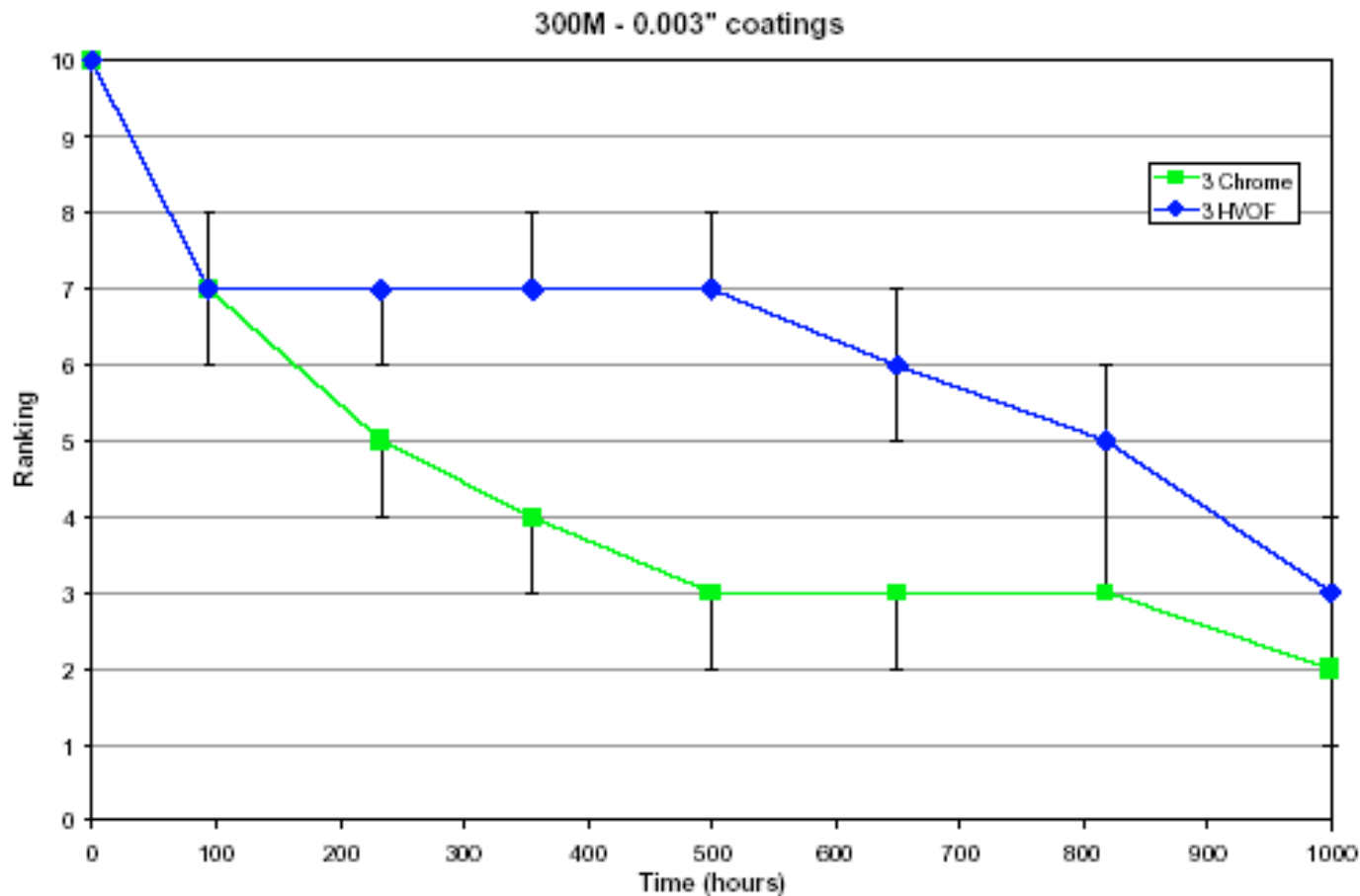
# HVOF and Cr after 3 yr beach exposure and cleaning



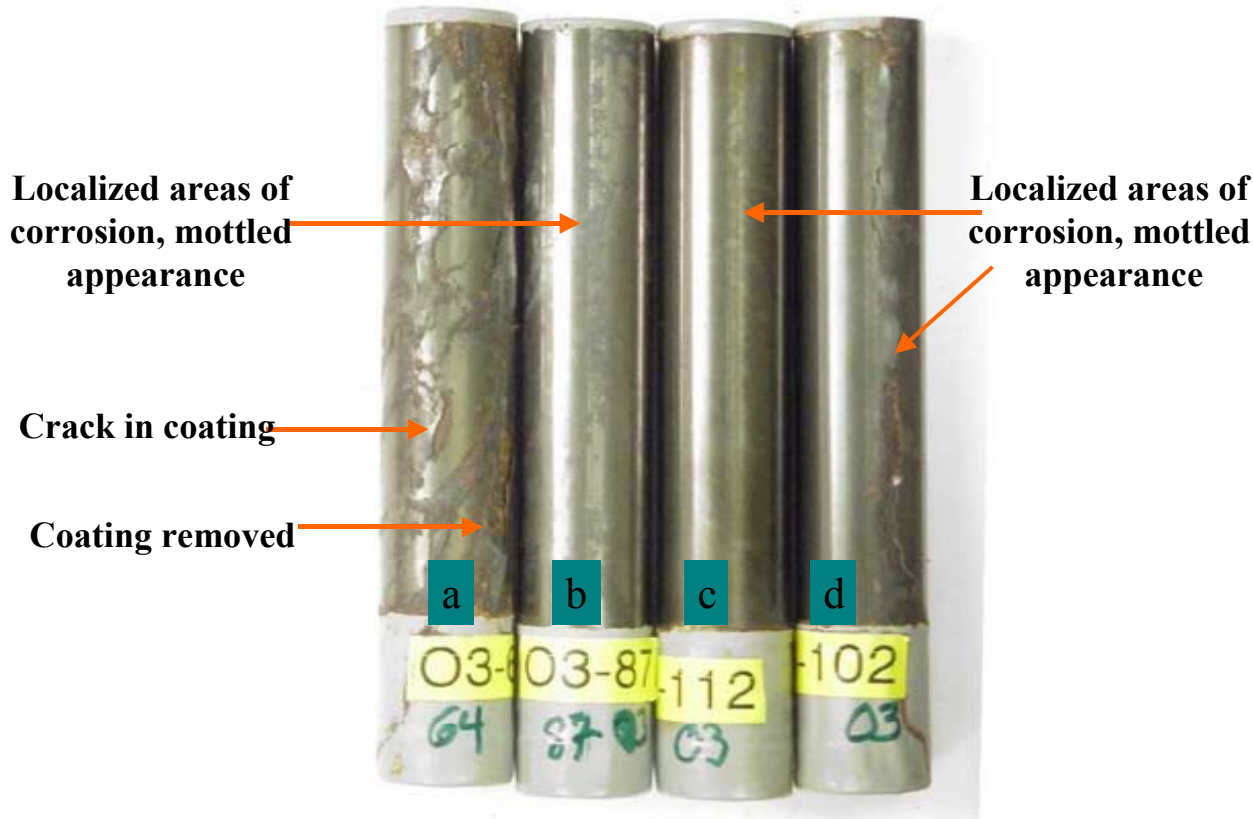
# Corrosion - GM test data



# C-HCAT data



# HCAT B117 on rods not consistent



- Reason for inconsistency still being evaluated

HVOF coatings on 4340 steel after the B117 test : a) 3mil WC/Co, b) 10 mil WC/Co, c) 10 mil WC/Co-Cr, and (d) 3 mil WC/Co-Cr

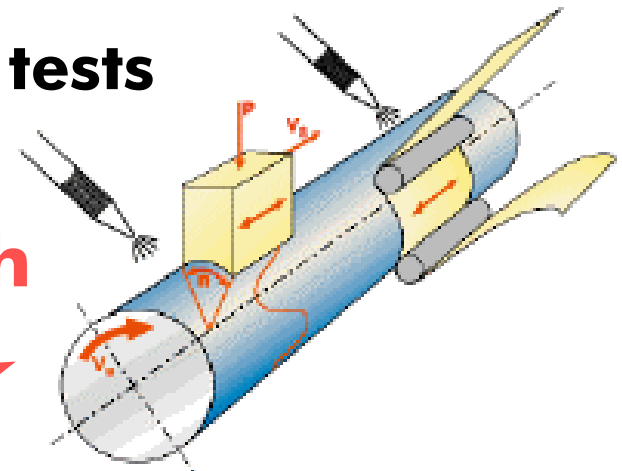
# Corrosion summary

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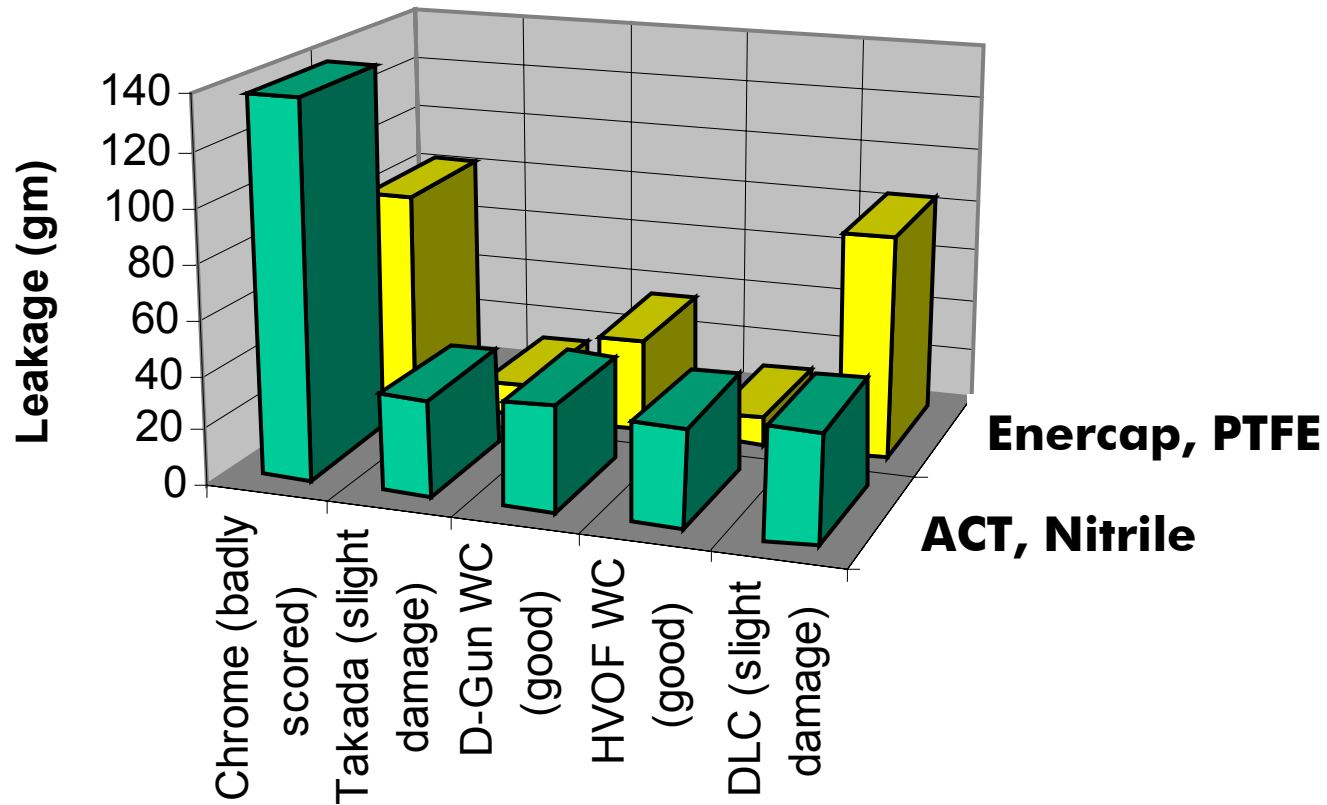
- **Lufthansa, Delta and most other commercial users have chosen WC-CoCr for landing gear because of better corrosion performance**
- **All flight experience shows good corrosion**
- **Beach exposure shows good corrosion**
- **C-HCAT results show HVOF **better** than Cr**
- **Most lab data shows HVOF coatings to be better in corrosion than chrome**
  - **Latest HCAT B117 and B117-SO<sub>2</sub> show HVOF worse**
    - **inconsistent with B117 and beach exposure**
    - **may be a testing problem**

# Wear

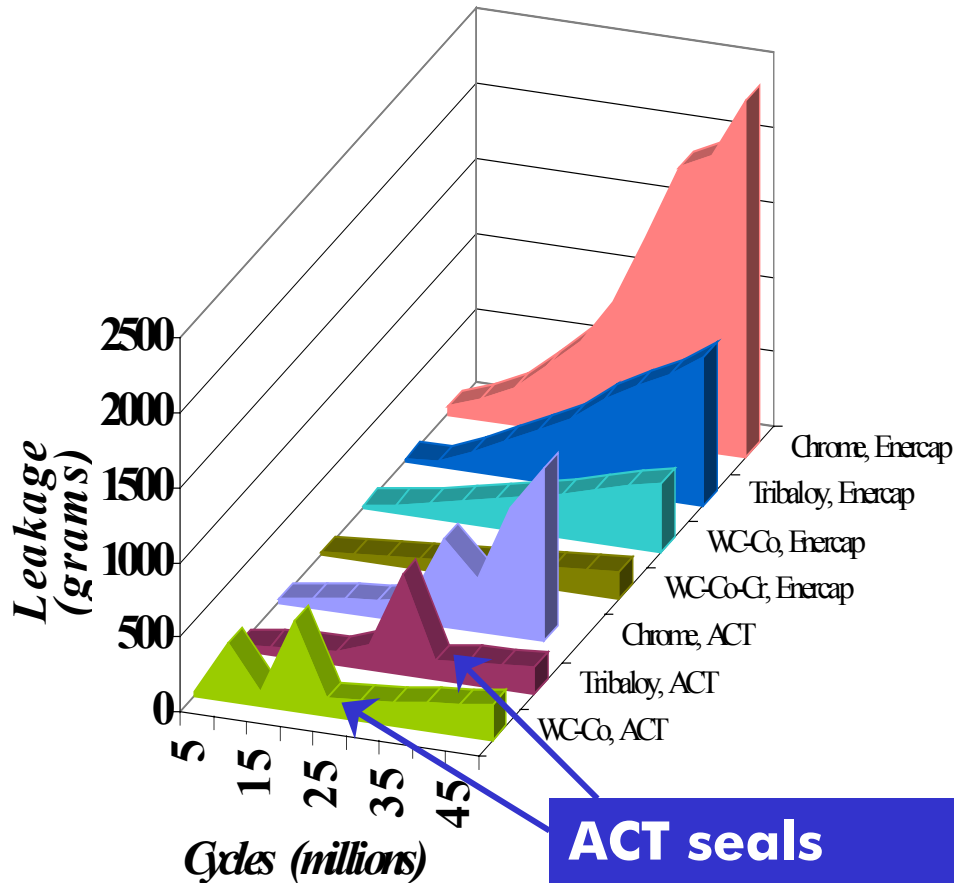
- **HVOF WC-Co and WC-CoCr are hard**
  - HVOF typically 1200-1400 HV
  - EHC typically 800-1000 HV
- **In the field HVOF wear life is usually at least 3xEHC**
  - No measurable wear in flight tests
  - Most scoring eliminated
- **Critical issue is surface finish**
  - Should generally be  $< 4\mu''$
  - May need superfinishing



# Hydraulic rig tests - initial low cycle Green, Tweed tests



# Hydraulic rod testing - Green, Tweed



**ACT seals replaced with**

- 50 million cycles
- Enercap (PTFE seal)
- ACT (Nitrile seal)
- Cumulative leakage
- No HVOF rod wear
- HVOF works well with PTFE seals

Surface finish:

EHC	4 μ" Ra
T 400	9 μ" Ra
WC-Co	4 μ" Ra
WC-CoCr	6.5 μ" Ra

# Hydraulic testing summary

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- **Surface finish must be  $<4\mu''$  or superfinished**
  - **Every attempt to use typical chrome  $16\mu''$  in rig or flight tests has caused rapid seal wear**
- **WC-Co and W-CoCr work well on flight surface-type actuators with PTFE seals, but tend to damage nitrile seals**
  - **However, in landing gear flight tests (and presumably utility actuators), nitrile seals work well**
- **T400 works better than chrome, but more wear than WC**

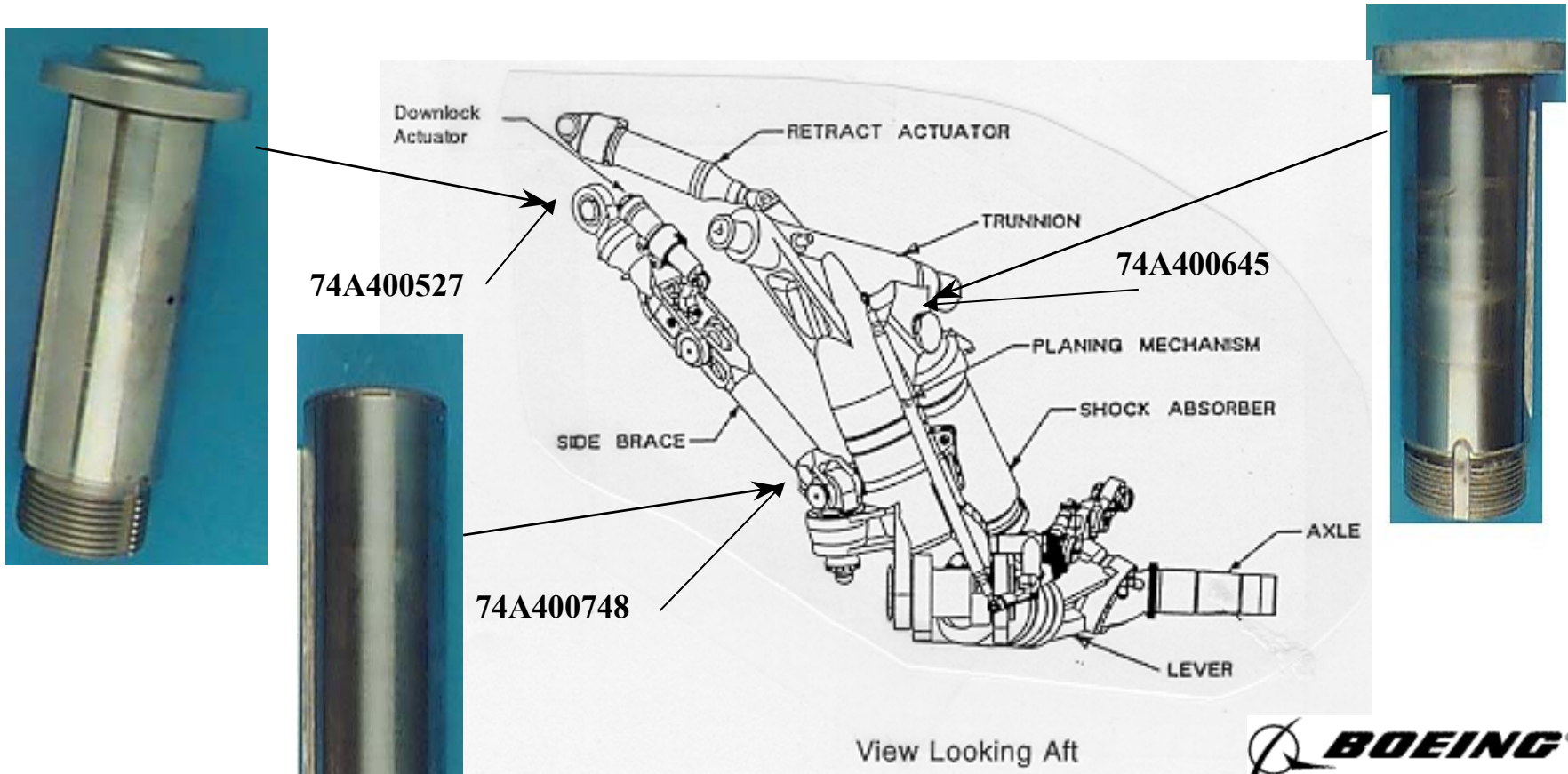
# Critical issue with all hydraulics

## ■ Surface finish is critical!

- The most wear resistant coating in the world is worthless if it just wears out the seals



# F-18 E/F landing gear rig test - HVOF WC-17Co pins after 14,000 SFH



 **BOEING**  
tests

**Passed, better than Cr  
But need full scale rig**

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# Flight tests

- **Commercial flight tests by Lufthansa, Boeing, 2-year Delta**
  - **All successful - little or no wear on pistons or axles, or seals (when superfinished)**
- **Landing gear flight tests**
  - **P-3 Orion (Navy, under way)**
  - **EA-6B (Navy, awaiting OK)**
  - **Dash 8 (Bombardier, plan)**
  - **C-130 (Canadian Air Force, plan)**



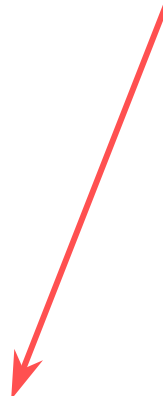
# Finishing, stripping

## ■ Finishing

- **Must grind with diamond wheel**
- **Superfinishing removes debris**
- **Small level of porosity appears to hold fluid**

## ■ Stripping of WC

- **Standard electrochemical Rochelle salt - benign**
- **Cannot be water jet stripped**
- **T400 difficult to strip - no simple methods**



Component	Value	Notes
Anhydrous sodium carbonate	20 - 30 oz/gal water	
Sodium potassium tartrate (Rochelle Salt)	8 - 12 oz/gal water	
Temperature	104 - 150°F	130 -150 °F optimal
pH	11 - 12	
Voltage	4 - 6 V DC	
Current density	4 - 8 A/sq in	Parts are anodic (positive)

# Other interesting issues

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- **Appears to be very difficult to grind burn**
  - **very low thermal conductivity**
    - **Might well prevent axle burn on stopping**
- **Looks as though will be able to rebuild to 0.060" by use of duplex coatings (e.g. build up with NiAl, cap with WC-Co)**
  - **Equivalent to sulfamate Ni + chrome**
  - **Requires no grinding of build-up layer**

# Conclusions

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- **HVOF works better than chrome in almost all respects**
- **Cost of HVOF 1 - 1.5x EHC**
  - **Likely much lower life-cycle cost - less wear**
- **Remaining issues**
  - **Corrosion data need to be clarified**
  - **Coating integrity - spalling at high load and R ratio issue to be resolved for use on landing gear pistons, especially on carrier-based aircraft**
  - **pins and axles are fine**

# Critical issues with use of HVOF

## ■ Process development

- **Process must produce coating to match application**
  - ❑ **Must optimize properly for the most important properties**
    - **Don't use a wear coating for a fatigue application**
- **Proper specs**
  - ❑ **Must specify structure, porosity, substrate temperature, stress**
  - ❑ **Grinding, finishing**

## ■ Process control

- **Deposition conditions**
  - ❑ **Stable, well-controlled equipment**
  - ❑ **Particle velocity, temperature**
  - ❑ **Coating stress**
- **Temperature of component**

## ■ NDI for cracks in steel

- **FPI, Barkhausen work**
- **Eddy current can work, but must be very sensitive**
- **MPI does not work**

## Use of Thermal Spray as an Aerospace Chrome Plating Alternative



Courtesy U.S. Navy. Photo by Design John Gray

Report to:  
William Green  
Geo-Centers

Rowan Project #: 3105JSF3

Contract Number: N00173-98-D-2006, D.O. 0002  
Subcontract Number: GC-3363-99-004  
P.O. Number: 28578MK

Report Number: Final

Date: October 27, 2000

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